

Numerical simulation of powder snow avalanches

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« Variabilité des phénomènes et des milieux naturels »



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Outline

- 1 Physical context
- 2 Mathematical modelling
- 3 Numerical results
- 4 Perspectives and conclusions

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Powder-snow avalanches

Large scale turbidity currents descending slopes at high velocities

Characteristic values :

Height : $H \sim 100$ m

Front velocity : $U_f \sim 100$ m/s

Density : $4 \text{ kg/m}^3 \leq \rho \leq 25 \text{ kg/m}^3$



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FIG.: Protecting wall in armed concrete at Taconnaz

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Mathematical models

Classification of various existing approaches

- Probabilistic / **Deterministic** models
- Discrete
 - granular material
 - cellular automata
- **Continuous**
 - 0D : conservation laws expressed as ODEs (Kulikovskiy & Sveshnikova (1970), Beghin (1979))
 - 2DH : depth integrated equations (Savage-Hutter)
 - 3D : Free-surface flow
 - 3D : **Two-fluid simulations** (DNS)

« + » : Both fluids are resolved

« + » : Flow structure is completely determined

« - » : Simulations are expensive

- Limited to relatively simple situations

Mathematical model

J. Etienne, P. Saramito, E.J. Hopfinger. Numerical simulations of dense clouds on steep slopes : Application to powder-snow avalanches. Annals of Glaciology, 38, (2004)

- Flow of two miscible fluids : ϕ – the volume fraction

$$\rho = \phi\rho^+ + (1 - \phi)\rho^-, \quad \mu = \phi\rho^+\nu^+ + (1 - \phi)\rho^-\nu^-$$

- Flow is incompressible

$$\nabla \cdot \vec{u} = 0$$

- Two fluids share the same velocity \vec{u}

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla)\vec{u} + \frac{\nabla p}{\rho} = \vec{g} + \frac{1}{\rho} \nabla \cdot (2\mu \mathbb{D}(\vec{u}))$$

- Mixing is modeled by Fick's law

$$\frac{\partial \phi}{\partial t} + \vec{u} \cdot \nabla \phi = \nabla \cdot (\nu_f \nabla \phi)$$

Kinetic energy balance equation

$$\frac{d}{dt} \frac{1}{2} \int_{\Omega} \rho |\vec{u}|^2 d\Omega = \int_{\Omega} \frac{|\vec{u}|^2}{2} \nabla \cdot (\nu_f \nabla \rho) d\Omega + \int_{\Omega} \rho \vec{g} \cdot \vec{u} d\Omega - \int_{\Omega} 2\mu |\mathbb{D}(\vec{u})|^2 d\Omega$$

Important remark :

- When we add diffusion in mass conservation, momentum equation has to be **corrected**

Energetically consistent model :

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} - \nu_f \nabla \log \rho \cdot \nabla \vec{u} + \frac{\nabla p}{\rho} = \vec{g} + \frac{1}{\rho} \nabla \cdot (2\mu \mathbb{D}(\vec{u}))$$

$$\frac{d}{dt} \frac{1}{2} \int_{\Omega} \rho |\vec{u}|^2 d\Omega = \int_{\Omega} \rho \vec{g} \cdot \vec{u} d\Omega - \int_{\Omega} 2\mu |\mathbb{D}(\vec{u})|^2 d\Omega$$

Governing equations

Classical gravity current scaling

- Dimensionless form :

$$\begin{aligned}\nabla \cdot \vec{u} &= 0, \\ \frac{\partial \phi}{\partial t} + \vec{u} \cdot \nabla \phi &= \nabla \cdot \left(\frac{1}{\text{ReSc}} \nabla \phi \right), \\ \frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} - \frac{1}{\text{ReSc}} \nabla \log \rho \cdot \nabla \vec{u} + \frac{\nabla p}{\rho} &= \vec{g} + \frac{1}{\rho} \nabla \cdot \left(\frac{1}{\text{Re}} 2\mu \mathbb{D}(\vec{u}) \right)\end{aligned}$$

$$\rho := \phi + (1 - \phi) \frac{\rho^-}{\rho^+}, \quad \mu := \phi + (1 - \phi) \frac{\rho^- \nu^-}{\rho^+ \nu^+}$$

Four scaling parameters to be respected :

Reynolds Re ; Schmidt Sc ; Atwood At ; viscosity ratio $\frac{\nu^-}{\nu^+}$

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Numerical methods

Finite volumes method

Open  FOAM

The Open Source CFD Toolbox

Our solver is based on :

- `twoLiquidMixingFoam`
- This standard solver was **modified** to include the extra term
- Structured meshes
- Second-order upwind finite volumes scheme
- Implicit time discretization

Remark :

Excellent **local conservative** properties

Conservation issues with FEM

J. Etienne. PhD thesis, INPG, Grenoble (2004)

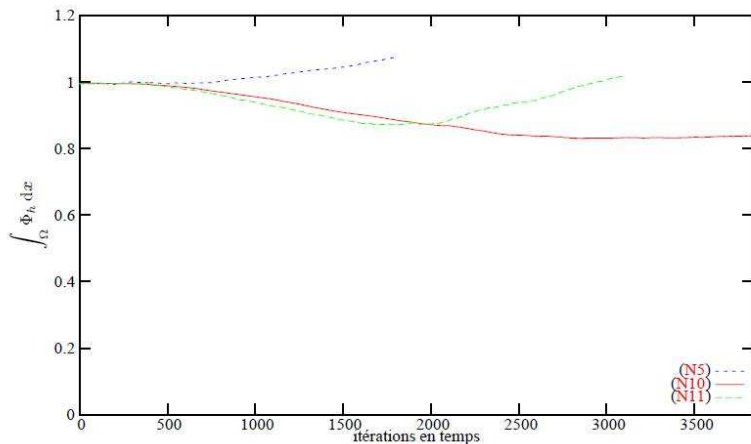


FIG. 31 – Conservation approchée de la masse.

Conservation issues with FEM

J. Etienne. PhD thesis, INPG, Grenoble (2004)

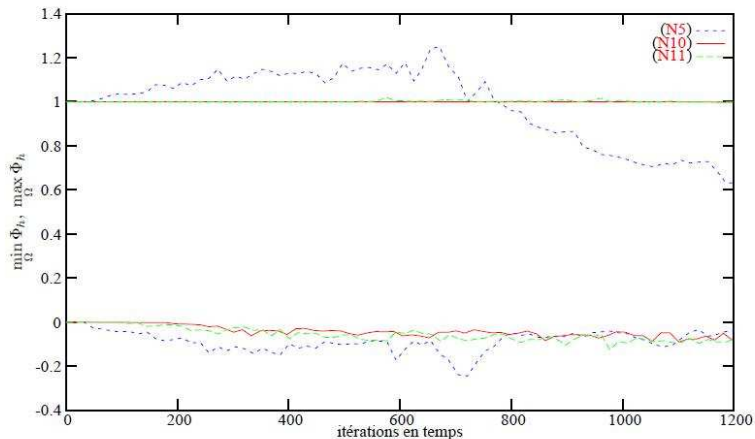
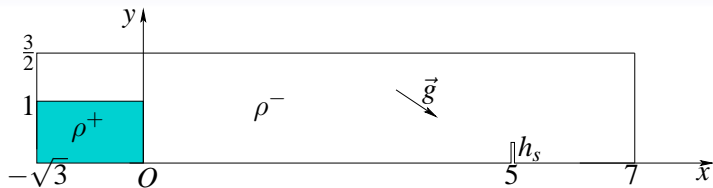


FIG. 32 – Principe du maximum approché : maximum de l'écart de Φ_h avec ses bornes supérieures et inférieures théoriques.

Sliding mass test-case

Classical lock-exchange type flow

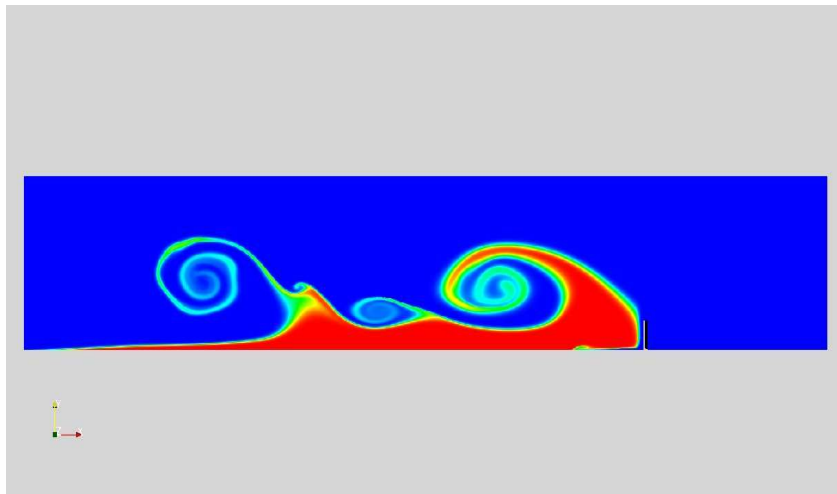


| <i>parameter</i> | <i>value</i> |
|---------------------------------|--------------|
| gravity acceleration $g, m/s^2$ | 9.8 |
| slope, θ | 32° |
| Reynolds number, Re | 10^5 |
| Schmidt number, Sc | 0.5 |
| friction parameter, α | 0.3 |
| initial mass height, h_0 | 1 |
| obstacle height, h_s | $0.25h_0$ |
| obstacle thickness | $0.05h_0$ |

| <i>parameter</i> | <i>value</i> |
|------------------|--------------|
| $\rho^+, kg/m^3$ | 4 |
| $\rho^-, kg/m^3$ | 1 |
| $\nu^+, m^2/s$ | 10^{-5} |
| $\nu^-, m^2/s$ | 10^{-5} |

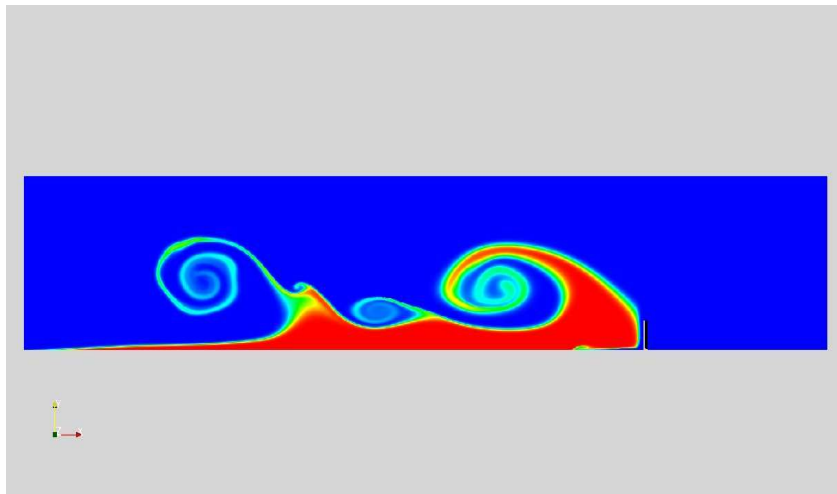
Sliding mass test case

Interaction with a « small » obstacle : $h = 0.25h_0$



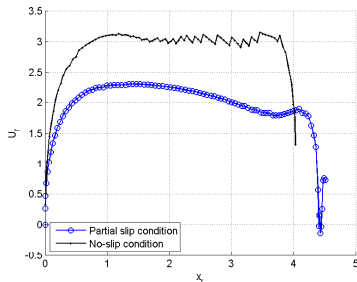
Sliding mass test case

Interaction with a « big » obstacle : $h = 0.6h_0$

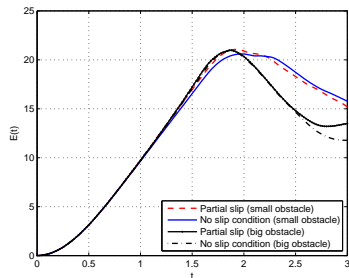


Computational results

Front velocity and kinetic energy



(a) Front velocity



(b) Kinetic energy evolution with time

Reference :

D. Dutykh, C. Acary-Robert, D. Bresch. *Numerical simulation of powder-snow avalanche interaction with an obstacle*. Submitted to Applied Mathematical Modelling (2009)

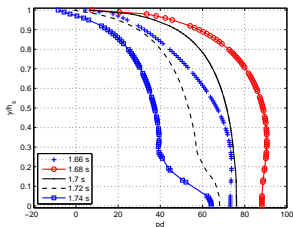
Impact pressures

Empiric and computational approaches

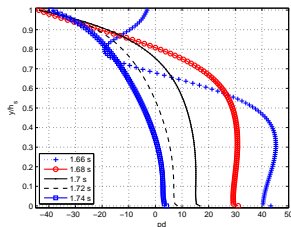
Empiric law (Beghin & Closet, 1990) :

$$p_d = \frac{K}{2} K_a(z) \bar{\rho} U_f^2, \quad K_a(z) = \begin{cases} 10, & z < 0.1h, \\ 19 - 90z, & 0.1h \leq z \leq 0.2h, \\ 1, & z > 0.2h, \end{cases}$$

Computation results :



(c) $h_s = 0.25h_0$



(d) $h_s = 0.6h_0$

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Conclusions and perspectives

Conclusions :

- We presented a two-fluid energetically *consistent* model
- Efficient and locally *conservative* scheme
- Allows for accurate computation of...
 - impact pressures
 - front position and velocity
 - kinetic energy loss
 - etc.

Perspectives :

- Comparison with **experimental** data
- Compressible effects
 - $Ma \approx 0.3$
- Realistic boundary conditions at the soil



Thank you for your attention !

<http://www.lama.univ-savoie.fr/~dutykh>